

1 2. LITERATURE REVIEW

2 2.1 Asphalt Recycling Figures

3 Currently, Belgium shows one of the highest exploitation rates of RA in Europe.
4 Although, rates concerned the total exploitation of the country are published annually, there are
5 no figures regarding the individual usage rates in the three regions of Belgium: Flanders,
6 Wallonia and Brussels. In TABLE 1, figures regards the volume of RA utilization in different
7 countries are presented, including Belgium [4], France [5], the Netherlands [5], the USA [6] and
8 Japan [6].

9 **TABLE 1: Production and RA rates in different countries.**

	Belgium	France	Netherlands	USA	Japan
Hot and warm mix production (10^6 tons)	3.30	35.40	9.70	331	55
Available RA amount (10^6 tons)	2.00	7.00	4.50	69.7	41.9
Exploitation of available RA in mixtures (%)	43.0%	64.0%	76.0%	91.0%	No data
Mixtures containing RA (%)	58.0%	65.0%	70.0%	No data	No data
Estimated average RA content (%)	45.0%	19.5%	50.4%	20.4%	47.0%

10

11 2.2 International experience

12 Many challenges appear when bituminous mixtures containing RA are being studied.
13 When RA is added in the mixture, two types of binder will be present: the aged RA binder and
14 the non-aged virgin binder. The interaction between the two types of binder is still under
15 discussion, without knowing the degree of blending between those [7]. A life-cycle assessment
16 (LCA) based research by Anthonissen [8] for Flemish mixtures, concluded that the
17 environmental benefits of adding RA in new asphalt mixtures are significant, recommending
18 though that the quality of the final mixture has to be ensured. Many researchers have studied the
19 influence of RA on the mechanical properties. The most important findings of a preliminary
20 research, regards to laboratory or field mixtures within a variety of RA content (25%-60%),
21 showed some similarities and some contradicted cases:

- 22 • Stiffness is increased along with the addition of RA [9-10].
- 23 • Fatigue is a contradicting factor for most cases. In some cases fatigue resistance show
24 improvements by the addition of RA [11-12]. On the other hand, West et al [13] showed
25 that fatigue cracking propagate more rapidly, on a field study that determined long-term
26 pavement performance.
- 27 • RA improves rutting performance because rutting is strongly connected to binder
28 viscosity [14]. By adding a hard binder, such as the aged RA binder, the viscosity
29 increases and as a result the rutting decreases. Laboratory tests [15-16] along with field
30 experiences [17] support this statement.
- 31 • The majority of researchers concluded that tailored made design must be taken into
32 account when RA is added [18-19].

1 3. MATERIALS AND METHODOLOGY

2 In Flanders, the production of asphalt mixtures must be aligned with the SB250 v3.1
3 regulations, provided and revised by the Flemish Road Agency (FRA). According to the
4 regulations, RA is prohibited for use in surface layers and depending on the mixture and/or the
5 type of the work (public or private) there are also limitations for base layers. Mixtures are
6 divided in building classes from B1 to B10, as for the most demanding to the less demanding
7 cases accordingly, in terms of the equivalent standard axles.

8 For this paper a dataset containing 74 registered asphalt mixtures in the wider area of
9 Flanders were analysed, provided by the FRA. Three types of asphalt mixtures are described in
10 this dataset: APO-A, APO-B and AVS-B. According to the Flemish Standards SB250, APO
11 stands for asphalt mixtures with performance requirements for base courses and AVS for asphalt
12 mixtures with increased stiffness. The corresponding types described in the European standards
13 are AC and EME accordingly. The A and B symbols describe the maximum size of stones,
14 namely for A stones up to 20mm and B up to 14 mm.

15 Each registration was handled as a unique observation containing the following
16 information: Stiffness (MPa), Fatigue ($\mu\text{m}/\text{m}$), Wheel rutting (%), RA content (%), total binder
17 content (%), old binder over new binder ratio (O/N) (%), air voids (VA) (%), virgin bitumen type,
18 final penetration, softening point (R&B) ($^{\circ}\text{C}$), stones (%), sand and filler (%). In some
19 registrations missing values were observed, hence those measurements were not considered as
20 part of the analysis. The objective of this research is twofold: first to shade light into the impact
21 of RA on the major mechanical properties by statistical means and secondly to provide insight on
22 the influential factors of those properties. Therefore, three statistical tools were used.

23 There are two methods in order to compare the two groups, mixtures with and mixtures
24 without RA, of the current data. The first test is the independent-samples T-test (parametric test)
25 and the second test is the Mann-Whitney U-test (non-parametric test). In order to perform a T-
26 test, the assumptions of normality and outliers non-presence must be met. In this study, the
27 normality has been assessed using as indicators the Shapiro Wilk test and graphically using the
28 Q-Q plots. Furthermore, the presence of outliers determined graphically, using boxplots. When
29 one of the aforementioned assumptions is violated, the Mann-Whitney U-test is used instead.
30 Continuous dependent variables included considered stiffness, fatigue and wheel rutting. The
31 comparison was conducted separately for all the three mixture types of the dataset: APO-A,
32 APO-B and AVS-B. The test was performed using the statistical software SPSS $\text{\textcircled{R}}$ v.24.

33 After the impact of RA had been assessed, the influential factors were determined.
34 Therefore, the strength of the association, between the continuous variables was expressed by
35 Pearson's correlation coefficient assuming a linear relationship. Moreover, a multiple linear
36 regression (MLR) analysis provided a model for the prediction of the mechanical properties
37 explained by the best fitted predictors, in this case properties of the mixture, composition and
38 binder characteristics. The multivariate and the MLR analysis were conducted for all the
39 mixtures of the dataset, to obtain one simplified model for each of the three mechanical
40 properties. The statistical software JMP Pro $\text{\textcircled{R}}$ v.12 was used for the multivariate and MLR
41 analysis.

1 **4. RESULTS**

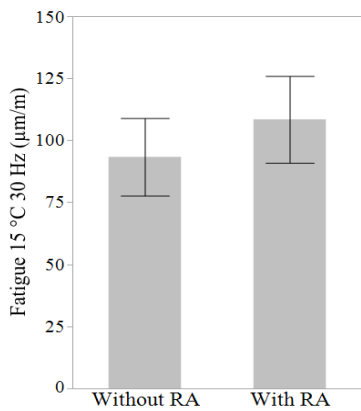
2 **4.1 Independent sample T-test**

3 First, to test whether the mean value of a continuous outcome variable differs between
 4 mixtures with and mixtures without RA, we carried out an independent-samples T-test
 5 (parametric) or a Mann-Whitney U test (non-parametric). In TABLE 2, the test results are
 6 presented. Summarizing the outcomes, significant differences ($p < 0.05$) were tracked for the
 7 following cases:

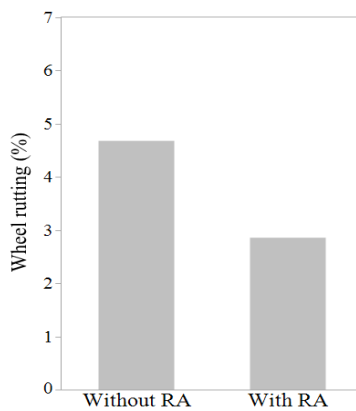
- 8 • The mean (M) fatigue resistance for APO-A mixtures with RA ($105.76 \pm 11.85 \mu\text{m/m}$) is
 9 significantly higher than mixtures without RA ($89.17 \pm 9.60 \mu\text{m/m}$) by $16.6 \mu\text{m/m}$, as
 10 assessed by the T-test: $t(27) = -3.157$, $p = 0.004$ (TABLE 2 and FIGURE 1).
- 11 • The median value of wheel rutting for APO-A mixtures with RA (2.86 %) is significantly
 12 lower than mixtures without RA (4.68 %) by 1.82 %, as assessed by the U-test: $U = 19$, z
 13 $= -2.18$, $p = 0.028$ (TABLE 2 and FIGURE 2).
- 14 • The mean (M) wheel rutting for APO-B mixtures with RA ($3.23 \pm 1.22 \%$) is
 15 significantly lower than mixtures without RA ($4.78 \pm 1.53 \%$) by 1.55 %, as assessed by
 16 the T-test: $t(19) = 2.340$, $p = 0.030$ (TABLE 2 and FIGURE 3).

17 **TABLE 2: T-test and U-test for mixtures with and without RA**

APO-A	RA	M	SD	T-test
Fatigue ($\mu\text{m/m}$)	Without With	89.17 105.76	9.60 11.85	$t(27) = -3.157$, $p = 0.004$
APO-A	RA	Medians	Mann-Whitney U test	
Wheel Rutting (%)	Without With	4.68 2.86	U 19.00	z -2.18
				p 0.028
APO-B	RA	M	SD	T-test
Wheel Rutting (%)	Without With	4.78 3.23	1.53 1.221	$t(19) = 2.340$, $p = 0.030$



19 **FIGURE 1: APO-A**
 20 **Fatigue mean values**



21 **FIGURE 2: APO-A**
wheel rutting median
values

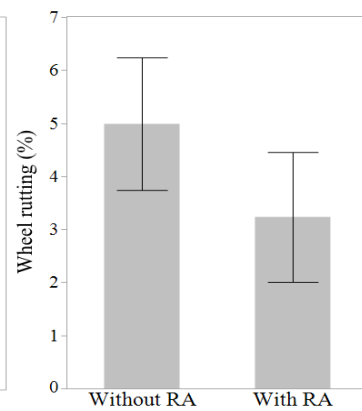


FIGURE 3: APO-B
wheel rutting mean
values

1 **4.2 Multivariate correlations**

2 The multivariate analysis provide information about the strength of the relation between
 3 the continuous variables. For the purpose of this research, the Pearson correlation analysis was
 4 used, to determine the strength and direction of a linear relationship between continuous
 5 variables. Therefore, the correlation between mechanical properties, i.e. stiffness (E^*), fatigue
 6 (ϵ_6) and wheel rutting (P_i), and material properties were. In TABLE 3 the Pearson’s correlation
 7 coefficients r can be found, including only the statistical significant pairs.

8 **TABLE 3: Pearson’s correlation analysis report**

		<i>RA</i> (%)	<i>Stones</i> (%)	<i>Sand</i> (%)	<i>VA</i> (%)	<i>O/N</i> (%)	<i>Total binder content</i> (%)	<i>Penetration</i> (dmm)	<i>Softening point</i> (°C)
E^* (MPa)	r	-	-	-	-	-	-	-0.416	0.320
ϵ_6 ($\mu\text{m/m}$)	r	-	0.482	-0.450	-0.417	-	0.623	-0.625	0.601
P_i (%)	r	-0.373	-0.369	0.365	-	-0.374	-	0.549	-0.574

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11 **4.3 Multiple linear regression**

12 Multiple linear regression model was fitted to predict the three major mechanical
 13 properties using as predictors material properties. First, all the available variables, concerning the
 14 mixture properties, were entered and then the final model was determined containing only the
 15 significant predictors ($p < 0.05$), following the backwards elimination procedure. The results of
 16 the analysis are:

- 17 • Stiffness was significantly predicted by the MLR model: $F(3,69)=7.339$, $p=0.0002$,
 18 adj. $R^2 = 0.210$. The regression coefficients and standard errors of the final predictors are
 19 presented in TABLE 5. The prediction expression is Eq. (1).
- 20 • Fatigue was significantly predicted by the MLR model: $F(2,71)=33.293$, $p=<.0001$,
 21 adj. $R^2 = 0.469$. The regression coefficients and standard errors of the final predictors are
 22 presented in TABLE 4. The prediction expression is Eq. (2).
- 23 • Wheel rutting was significantly predicted by the MLR model: $F(2,60)=21.962$, $p=<.0001$,
 24 adj. $R^2 = 0.403$. The regression coefficients and standard errors of the final predictors are
 25 presented in TABLE 6. The prediction expression is Eq. (3).

TABLE 5: Report of MLR analysis for stiffness

Variable	B	SE_B	p
Intercept	57658.678	16612.880	0.001
Stones	-474.051	190.789	0.015
Sand	-396.196	161.905	0.017
Penetration	-73.209	19.969	0.001

TABLE 4: Report of MLR analysis for fatigue

Variable	B	SE_B	p
Intercept	-64.997	22.293	0.005
RA	0.412	0.114	0.001
Binder content	33.812	4.151	<.0001

26

TABLE 6: Report of MLR analysis for wheel rutting

Variable	B	SE_B	p
Intercept	2.224	0.444	<.0001
O/N	-0.020	0.006	0.001
Penetration	0.064	0.012	0.0001

$$\text{Stiffness} = 57652.678 - 474.051 * (\text{stones } \%) - 396.196 * (\text{sand } \%) - 73.209 * (\text{penetration}) \quad (1)$$

$$\text{Fatigue} = -64.997 + 0.412 * (\text{RA } \%) + 33.812 * (\text{binder content}) \quad (2)$$

$$\text{Wheel rutting} = 2.224 - 0.020 * (\text{O/N}) + 0.064 * (\text{penetration}) \quad (3)$$

5. DISCUSSION AND CONCLUSIONS

In this work, mixtures produced in the wider area of Flanders were statistically investigated. During the first phase, the impact of RA on the three aforementioned mechanical properties was assessed. After that, a correlation was investigated between the material properties and the mechanical properties. The following conclusions have been derived from the current study:

- The analysed dataset consisted of mixtures that already met the performance requirements. Therefore, the potential benefits of RA are studied on properly designed mixtures. That was examined during the T-test/U-test analysis. In three outcome variables, wheel rutting and fatigue on APO-A mixtures and wheel rutting of APO-B mixtures, were significantly different when RA was added. For the other cases, no significant differences were traced.
- The T-tests/U-tests showed that the stiffness modulus does not change when moderate or high amount of RA is added, across all the mixtures. This result does not contradict the literature findings about improved stiffness when RA is implemented.
- The addition of RA has a negative linear correlation to the mixtures' wheel rutting. These results as well as the T-test result are fully in line with the international experience, as concluded by the literature review.
- The multivariate analysis also showed that the binder properties of the mixtures, i.e. penetration and softening point, significantly influence the current mechanical properties. Since RA replaces an adequate amount of the virgin binder, an improper blend design might mislead the mix design and consequently provide with low performance mixtures.
- Using the MLR analysis, three simple linear models were fitted. The adjusted R^2 of the models (0.210, 0.469 and 0.403) indicate that the data are rather spread around the regression line. Although, those models cannot accurately predict the mechanical properties, they can provide an insight into which factors mainly affect the mechanical properties.

The current results of this study indicated the impact that RA and other material properties have on the final behaviour of the mixture. Further research is needed in order to solidify the developed models. The examined dataset is annually updated, providing with the opportunity of creating an archive of manufactured mixtures in the Flemish region.

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